

Direct Geometry Processing for Tele-Fabrication

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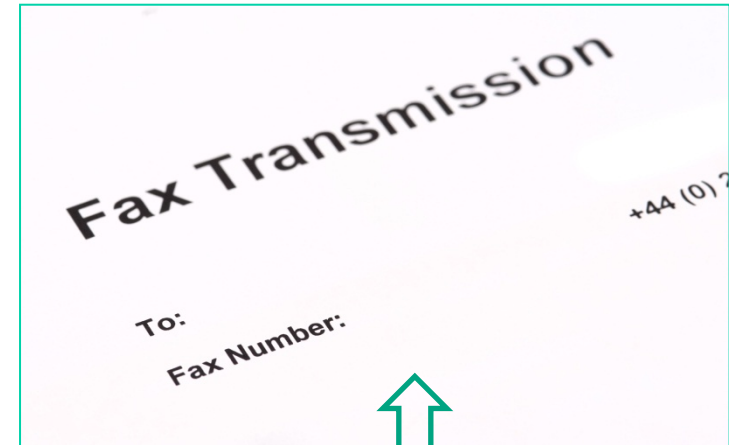
**2012 CIE Conference, Chicago, IL
Aug. 13, 2012**

- Introduction of 3D tele-fabrication
- 3D data acquisition
- Geometry processing
 - ❖ Point cloud slicing
 - ❖ Support generation
 - ❖ Mask image planning
- Fabrication results and discussion
- Summary

2D Faxing

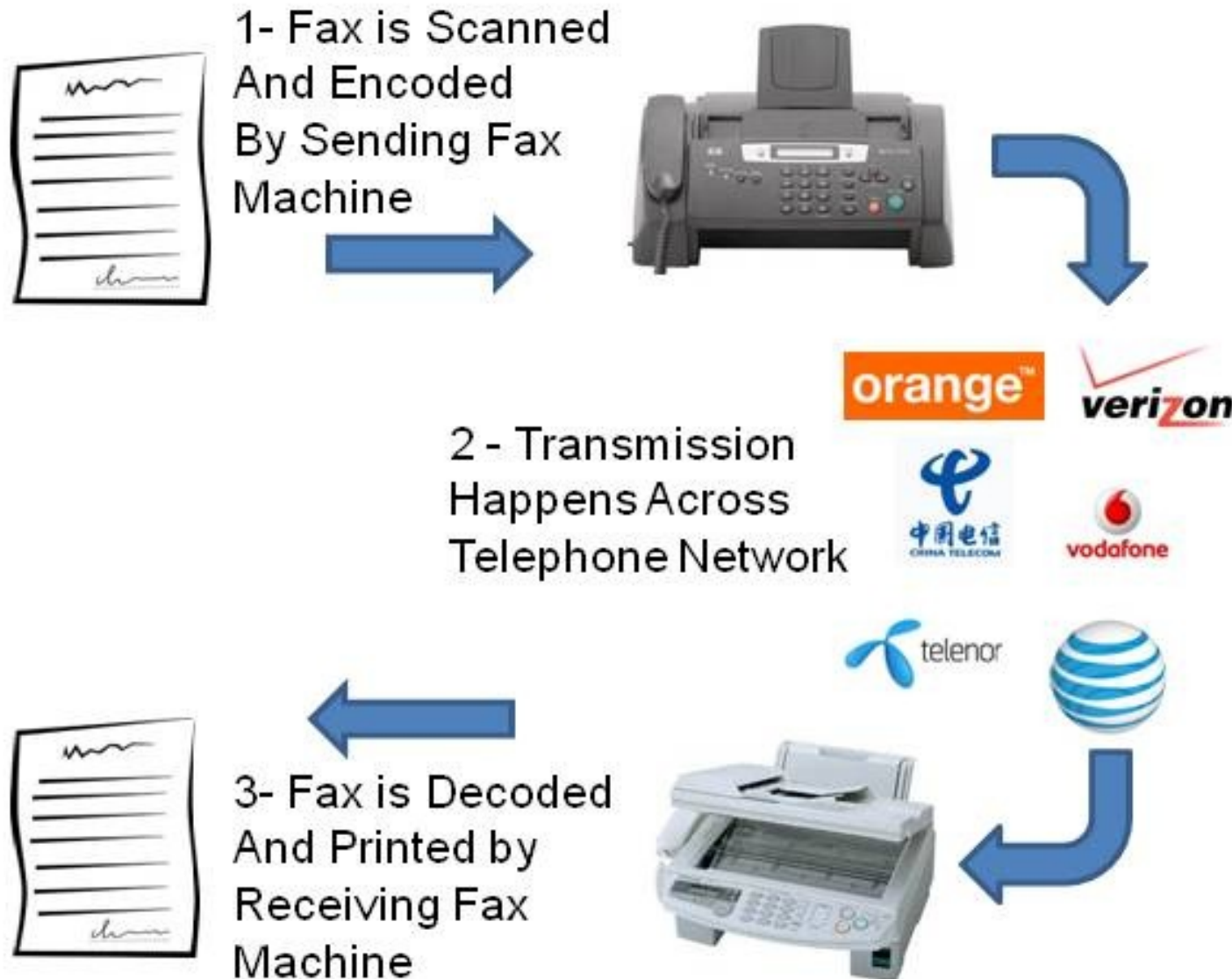


2D Scanning (Chicago)



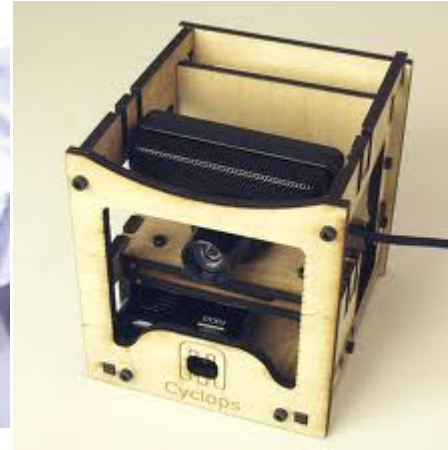
Printing (Los Angeles)

2D Faxing Processing



3D Scanners

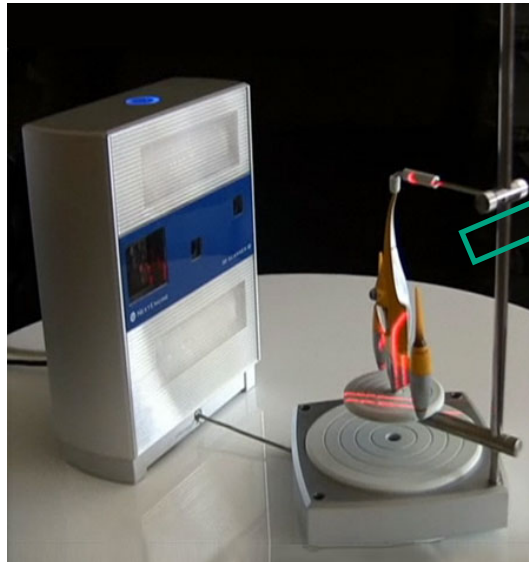
- Zcorp
- Makebot 3D replicator
- NextEngine
- 3Shape
- HDI 3D Scanner
- etc.



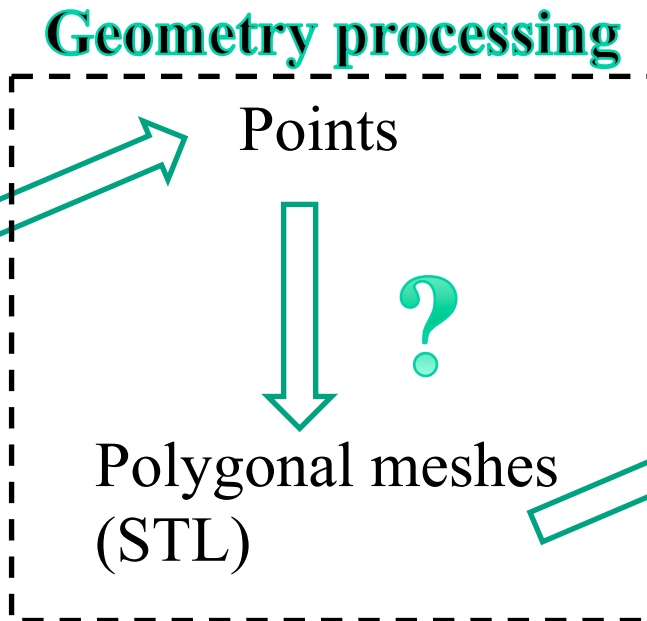
3D Printers

- Cubify
- VFlash
- Perfactory
- ZCorp
- Objet
- ProJet
- uPrint
- etc.





3D Scanners



3D Printers

- **An open question: how would geometry be processed in future 3D faxing systems?**

3D Tele-fabrication overview



3D Scanning
(Chicago)



Point cloud
slicing

Support
generation

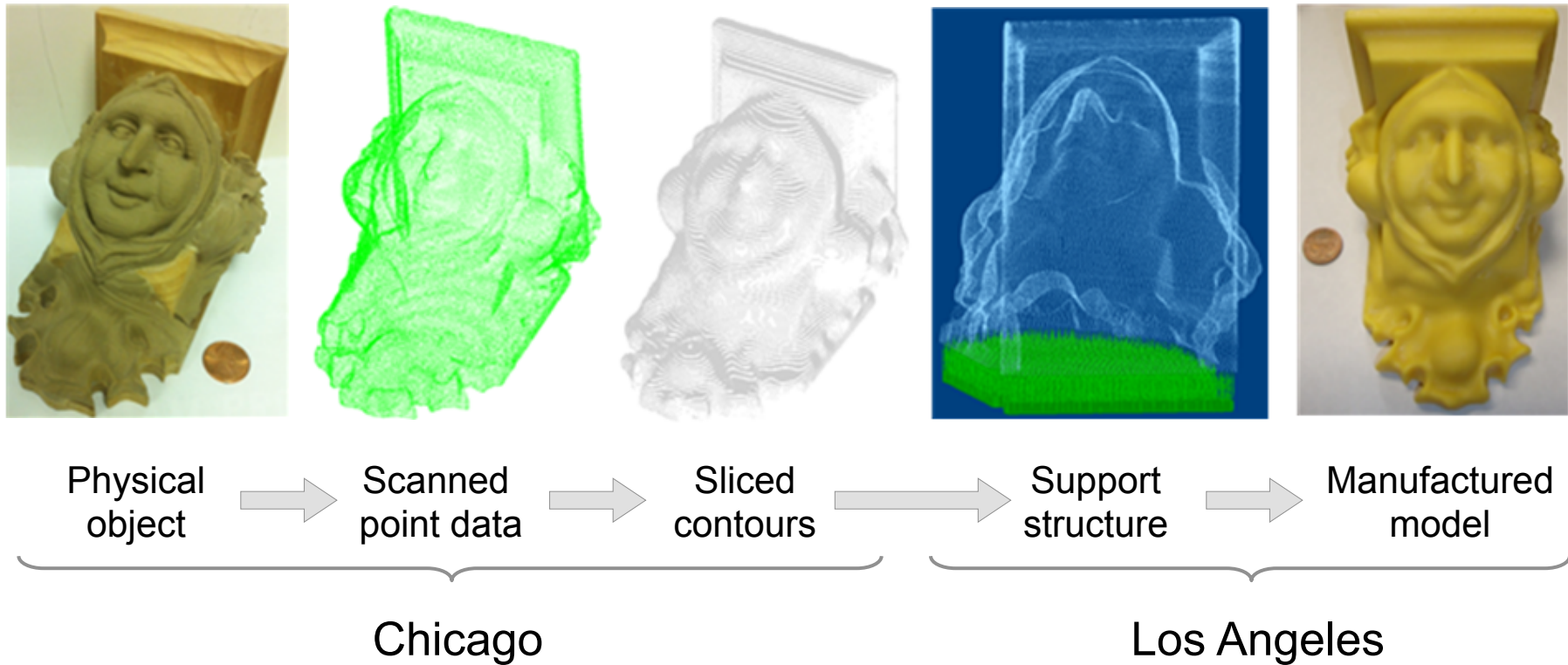
Mask image
planning

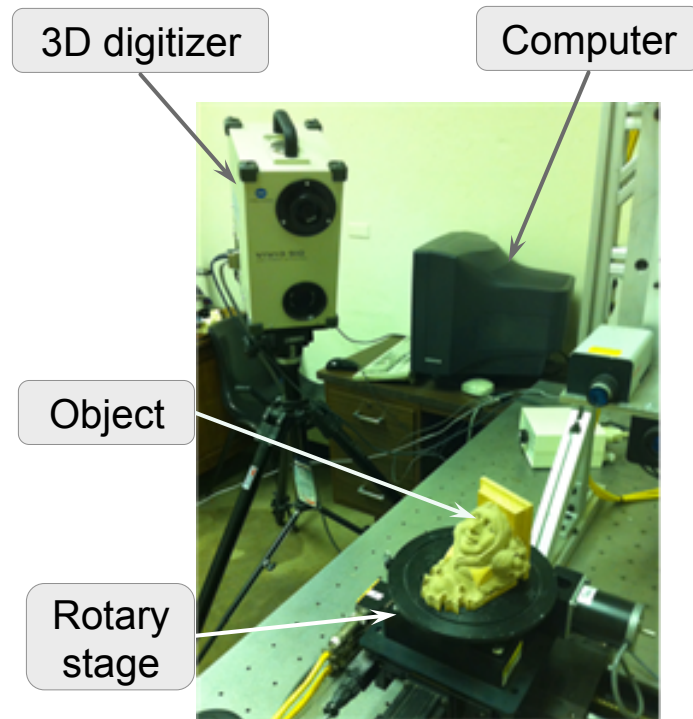
**Geometry
processing**



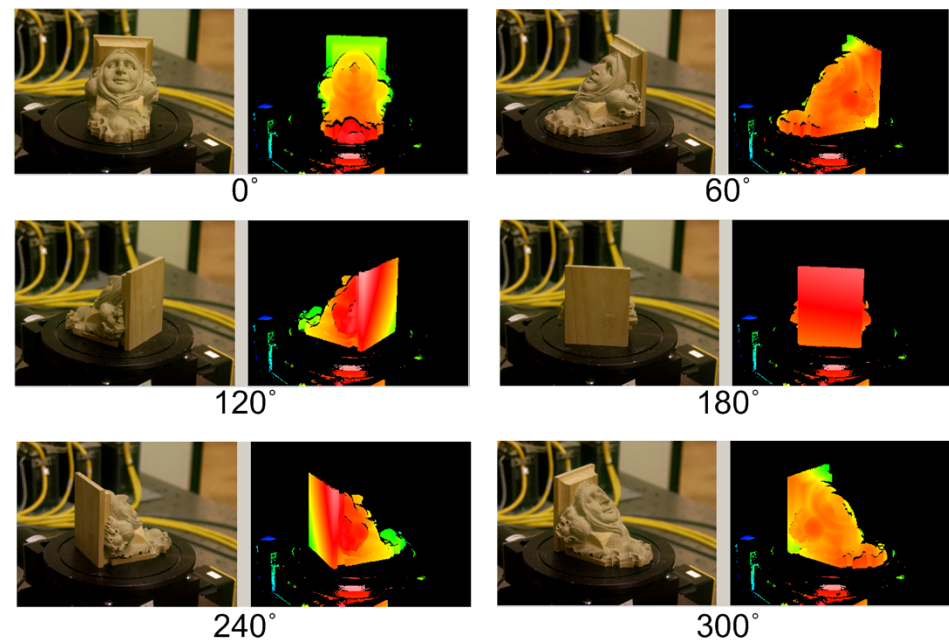
Manufacturing
(Los Angeles)

Geometry processing flowchart



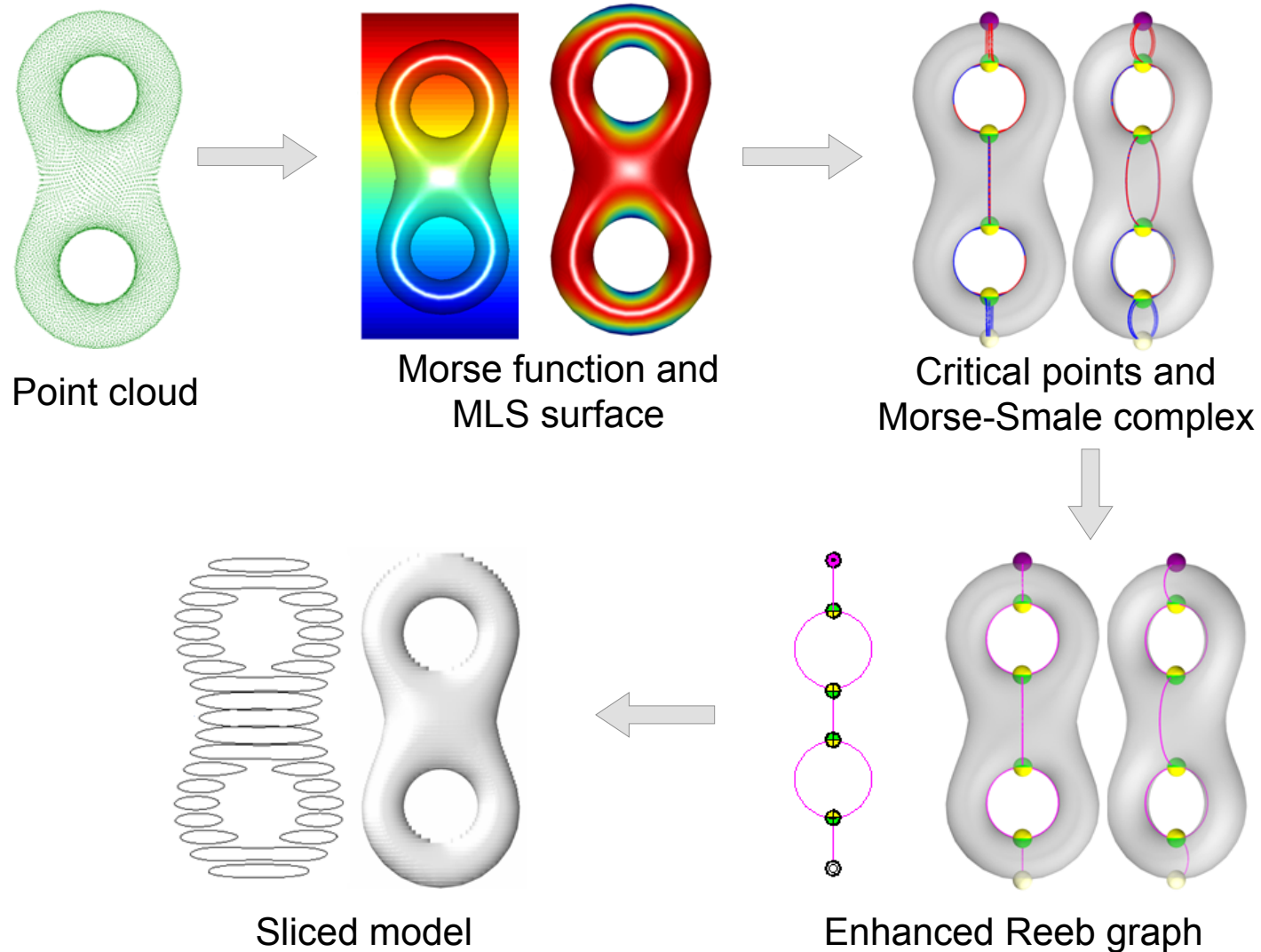


Digitizing system



6-step range image scanning

Point cloud slicing overview



Moving Least Square (MLS) surface

Implicit definition stationary set
of a projection operator

$$S = \{\mathbf{x} \in R^3 \mid \psi_p(\mathbf{x}) = \mathbf{x}\}$$

Energy function

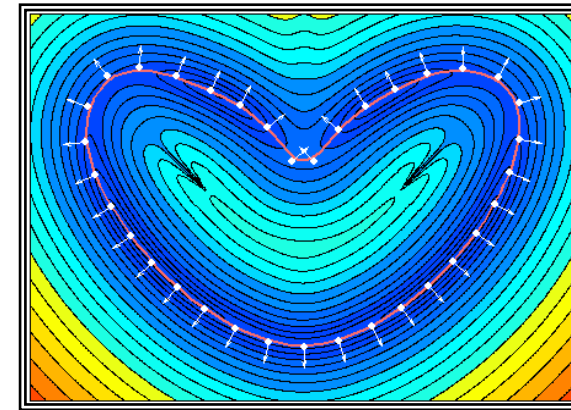
$$e(\mathbf{y}, \mathbf{n}(\mathbf{x}_i)) = \sum_{\mathbf{q}_i \in Q} ((\mathbf{y} - \mathbf{q}_i)^T \mathbf{n}(\mathbf{x}_i))^2 \theta_N(\mathbf{y}, \mathbf{q}_i)$$

Normal vector field

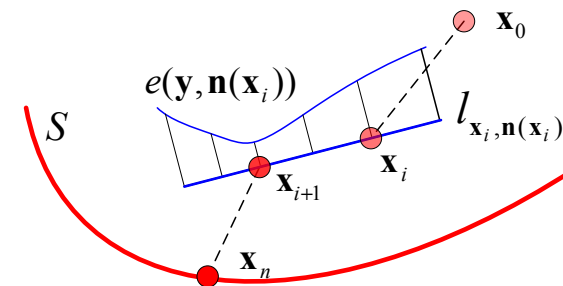
$$\mathbf{n}(\mathbf{x}) = \frac{\sum_{\mathbf{q}_i \in Q} \mathbf{v}_i \theta_N(\mathbf{x}, \mathbf{q}_i)}{\left\| \sum_{\mathbf{q}_i \in Q} \mathbf{v}_i \theta_N(\mathbf{x}, \mathbf{q}_i) \right\|} \quad \theta_N(\mathbf{x}, \mathbf{q}_i) = \frac{e^{-\|\mathbf{x} - \mathbf{q}_i\|/h^2}}{\sum_{\mathbf{q}_j \in Q} e^{-\|\mathbf{x} - \mathbf{q}_j\|/h^2}}$$

MLS explicit definition

$$g(\mathbf{x}) \equiv \mathbf{n}(\mathbf{x})^T \left(\frac{\partial e(\mathbf{y}, \mathbf{n}(\mathbf{x}))}{\partial \mathbf{y}} \bigg|_{\mathbf{y}=\mathbf{x}} \right) = 0$$



Energy function and
normal vector field



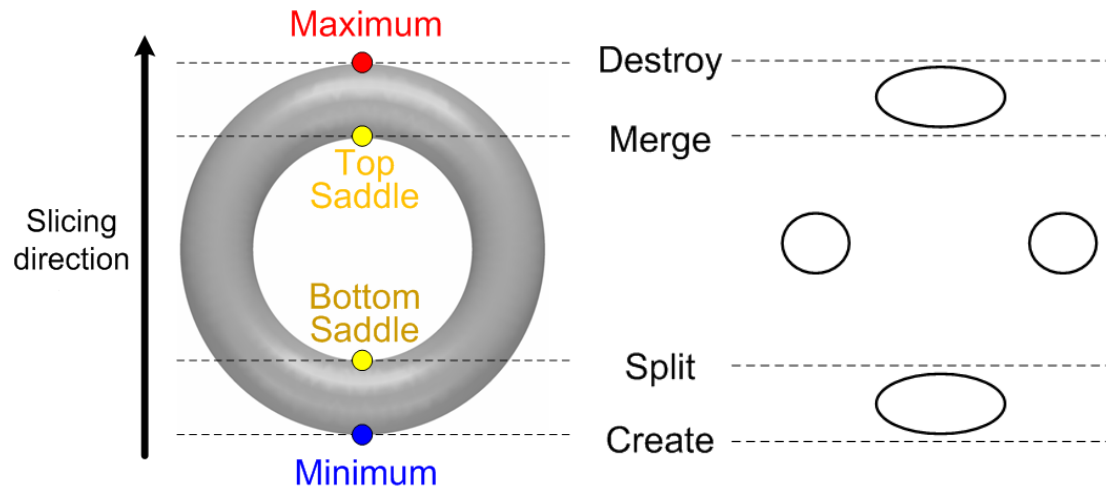
MLS surface point with
local minimum energy



Morse function
 f : height value



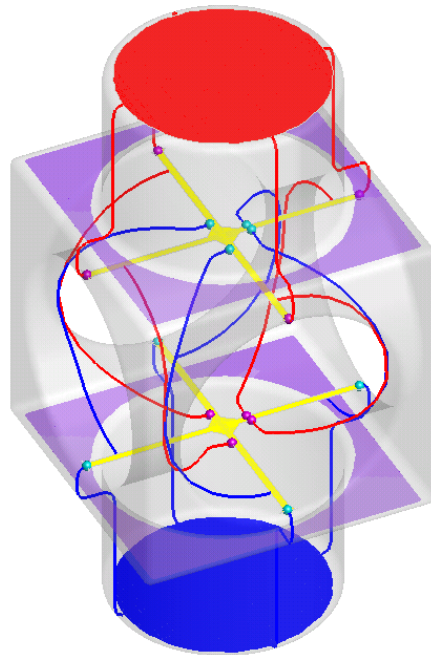
φ on MLS



4 types of critical points

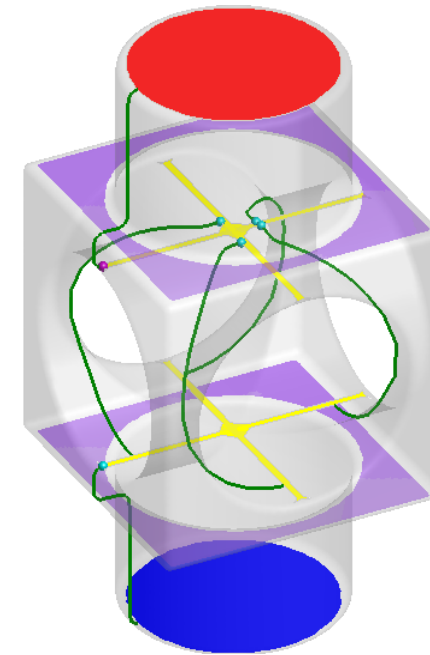
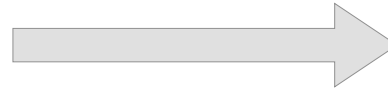
Contour topology

- Critical points identified by: $\varphi(\mathbf{x}) \equiv 1 - \left(\frac{\nabla f(\mathbf{x})}{\|\nabla f(\mathbf{x})\|} \cdot \frac{\nabla g(\mathbf{x})}{\|\nabla g(\mathbf{x})\|} \right)^2 = 0$
- Slicing contour topology controlled by critical points



MS complex:
integral lines tracing

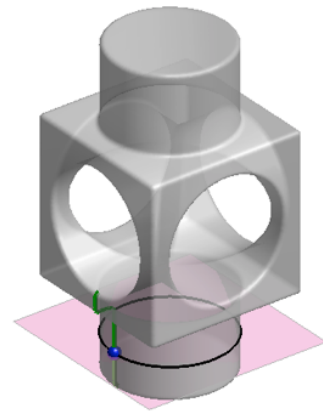
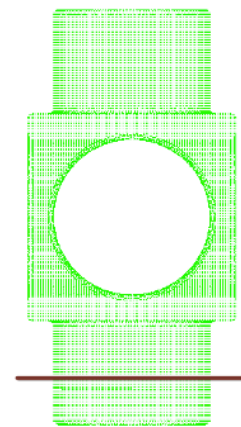
Grouping / Pruning



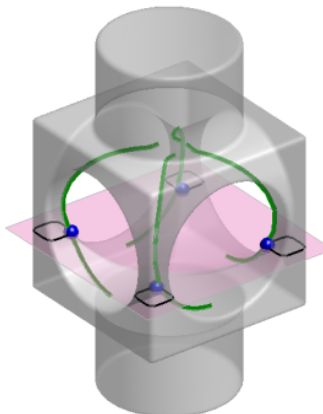
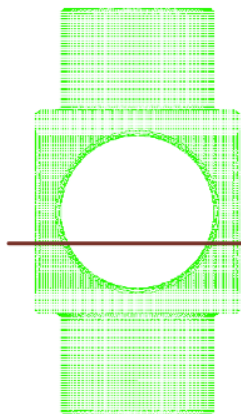
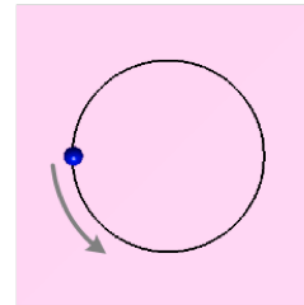
Enhanced Reeb graph:
MS complex re-organizing

- Morse-Smale (MS) complex: tracing integral lines from saddles to maximum/minimum
- Enhanced Reeb graph: graph processing of MS complex

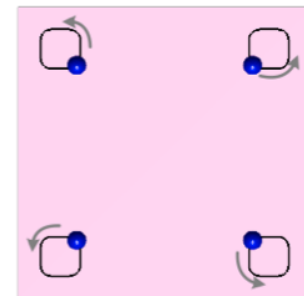
Enhanced Reeb graph as contour marching start



• Starting point
→ Marching direction



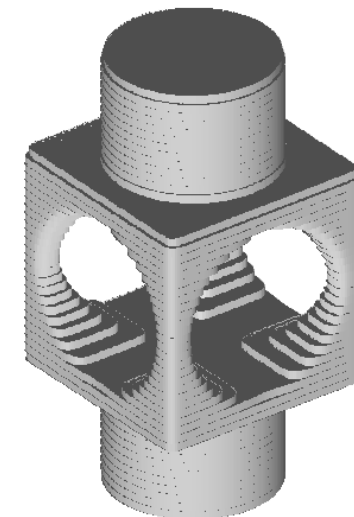
• Starting point
→ Marching direction



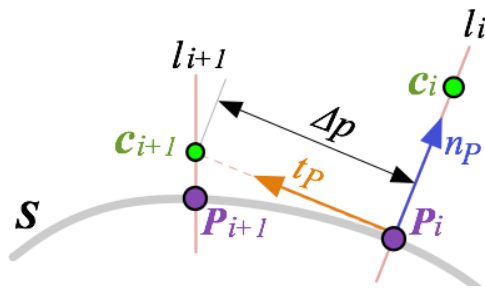
Slicing plane

Intersection with
enhanced Reeb graph

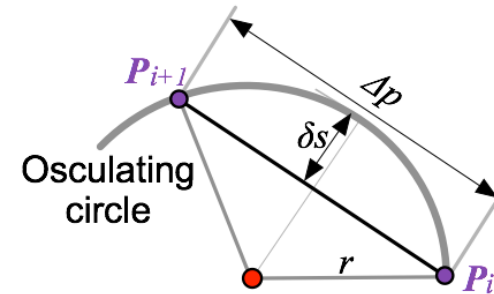
Contour marching from
intersected point



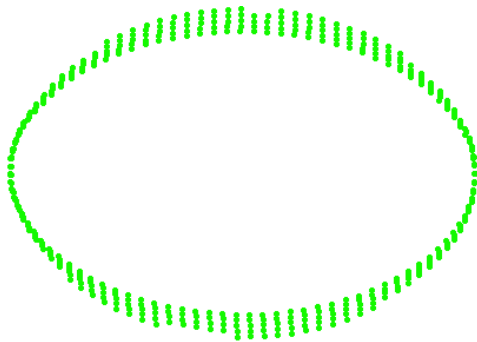
Sliced model: all raised
contours stacked



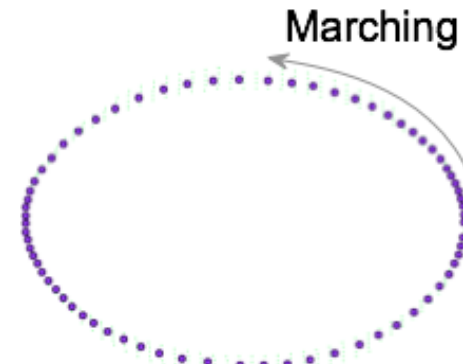
Contour marching by intersection



Curvature-adaptive step size



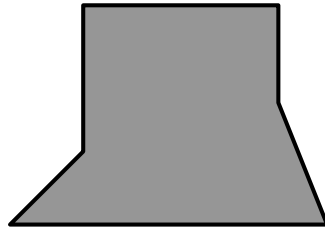
Point subset near the slicing plane



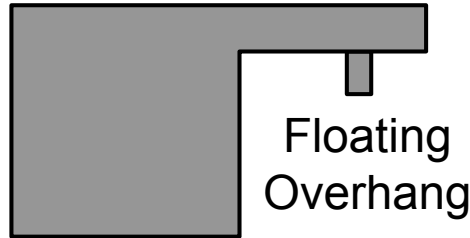
Adaptive contour points generation

- Step size determined by osculating radius

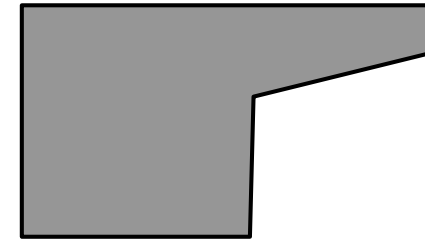
$$\Delta p = 2\sqrt{r^2 - (r - \delta_s)^2} = 2\sqrt{2r\delta_s - \delta_s^2}$$



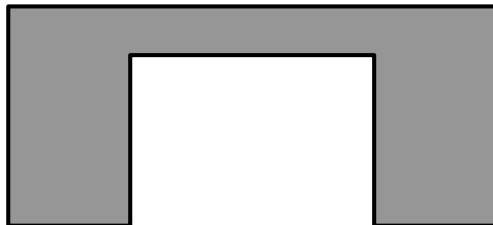
Flat Bottom



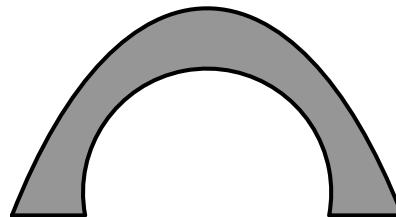
Floating
Overhang



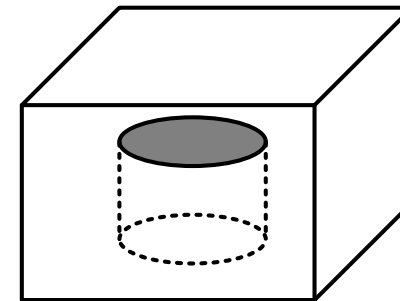
Cantilever



Cantilever



Vaulted Overhang



Ceiling

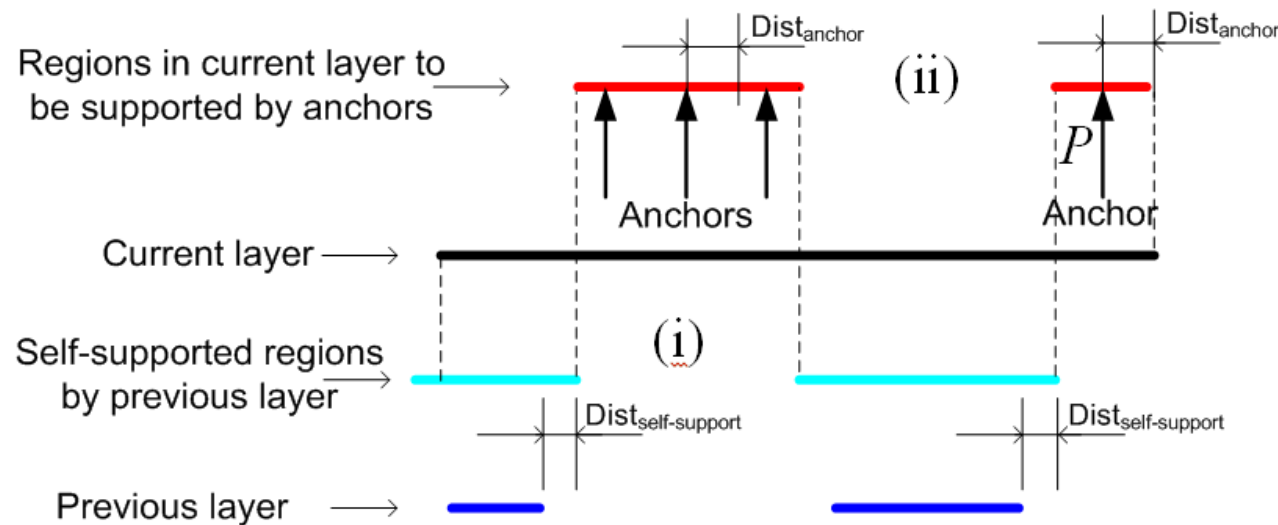
- Supports are required to ensure the success of the 3D printing process
 - No drifting/floating away;
 - Reduce deformation due to shrinkage.

Contour-based support generation principle

Current layer → 

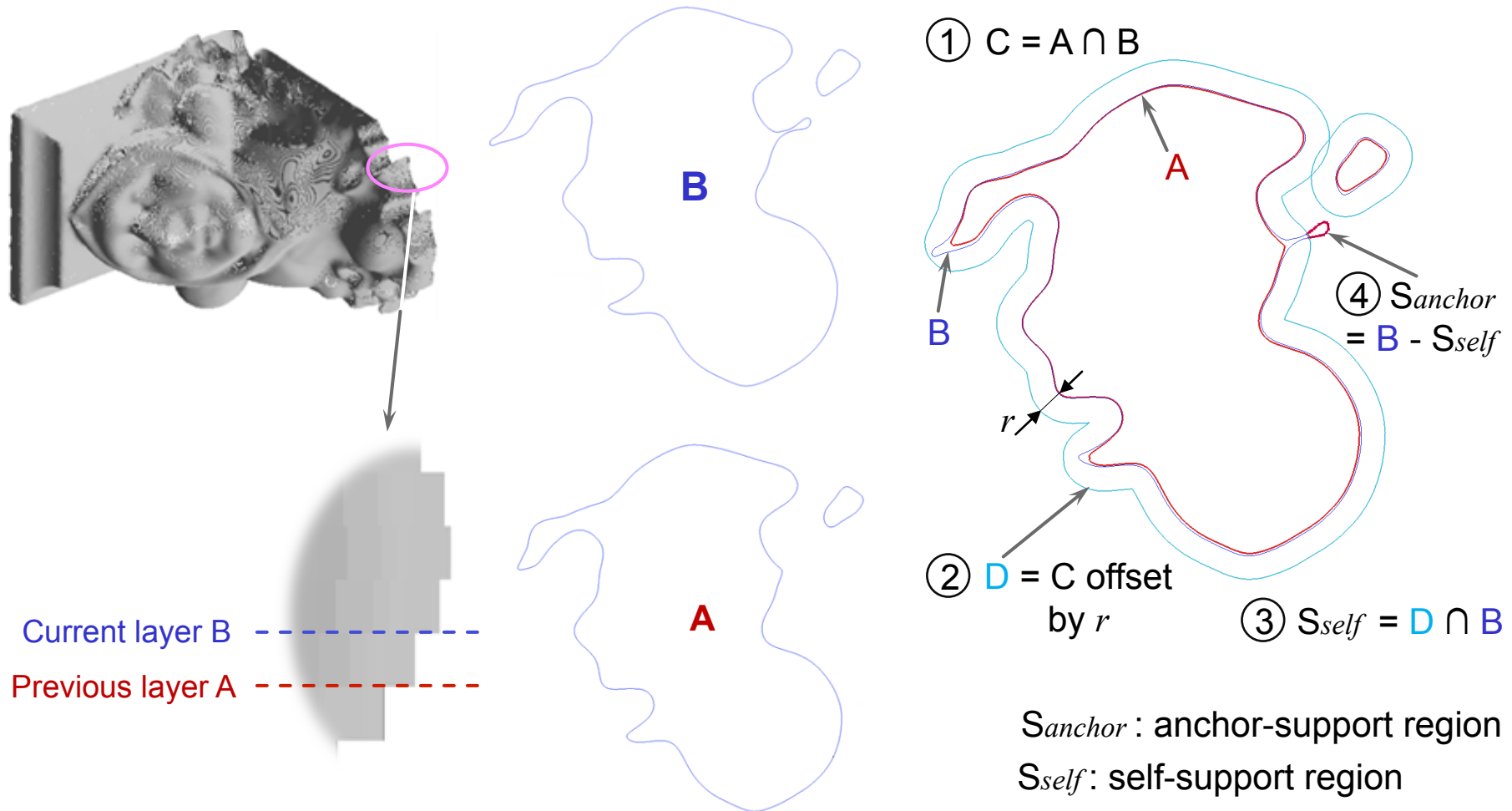
Previous layer → 

Two consecutive layer contours

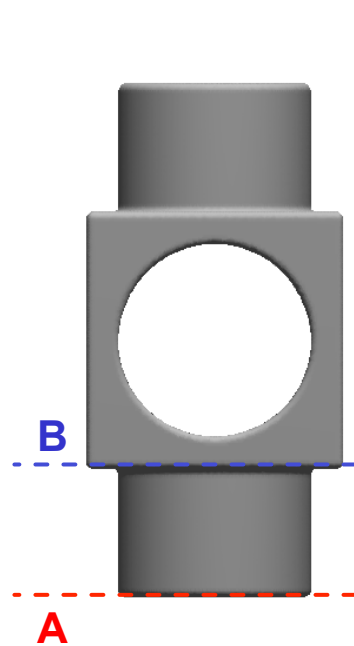


Support structure analysis

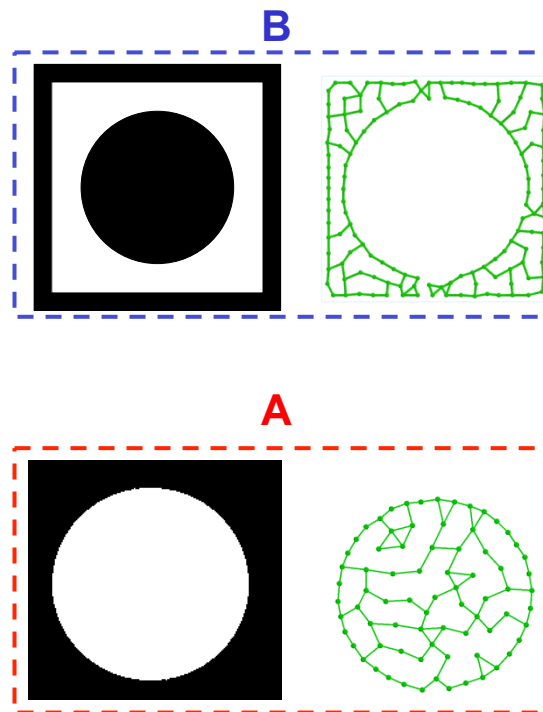
Support generation algorithms



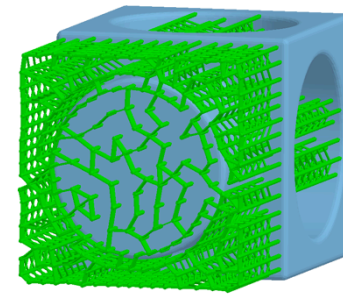
Anchor-support region covering



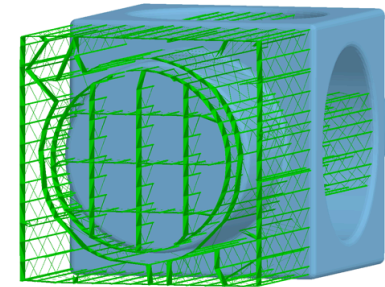
Input regions



Support layout by
region covering

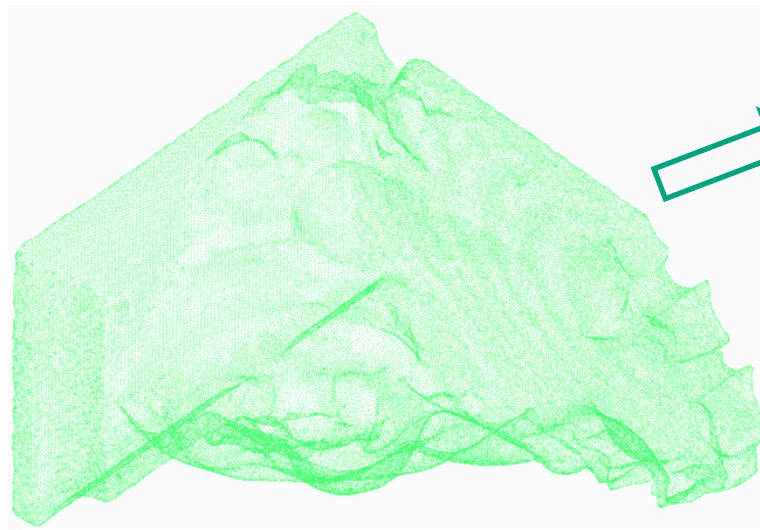


CAD model of
supports
(Contours based)



CAD model of support
by Lightyear system
(STL based)

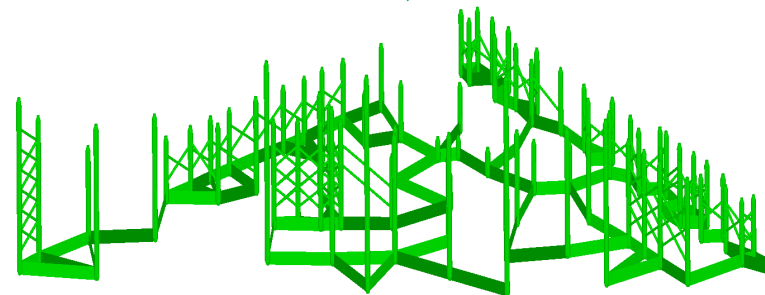
Support generation examples



Point cloud

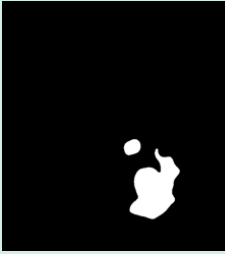
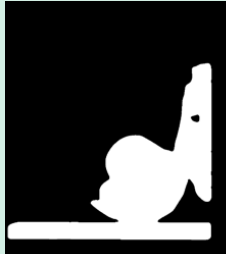
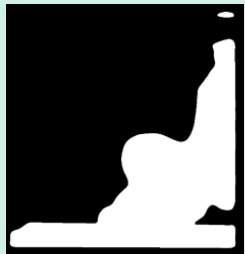
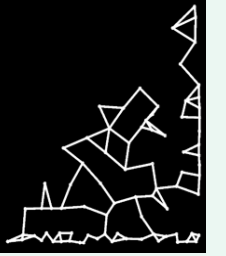
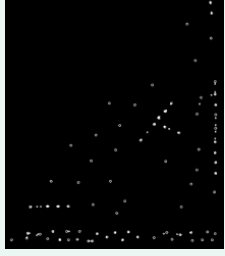
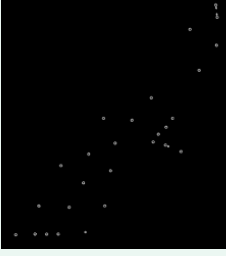



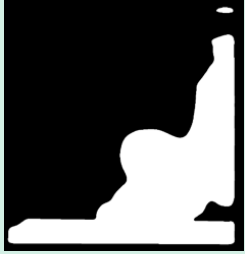


Sliced model



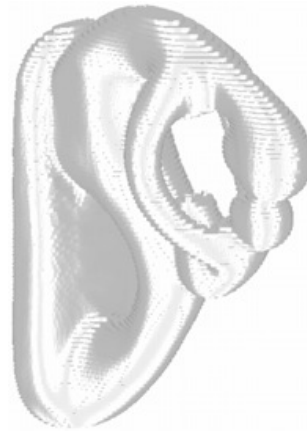
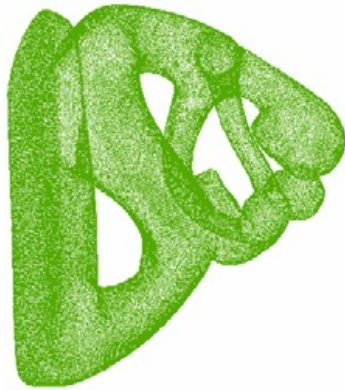
Support structure

Mask image planning: Image projection of layers

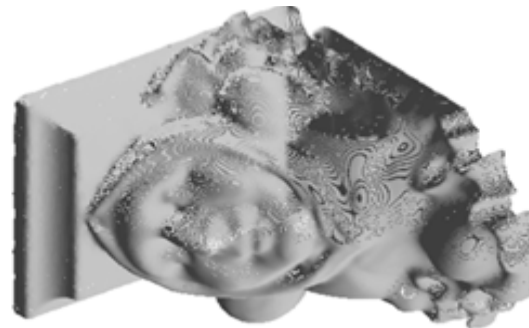
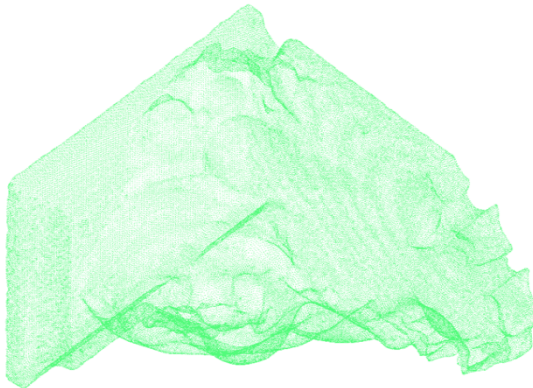
Layer ID	1	100	200	300
Mask image of part				
Mask image of support				
Projection mask image				

Fabrication example

(1)



(2)

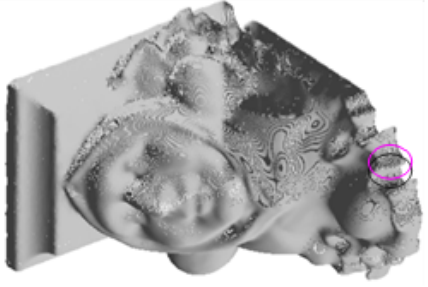



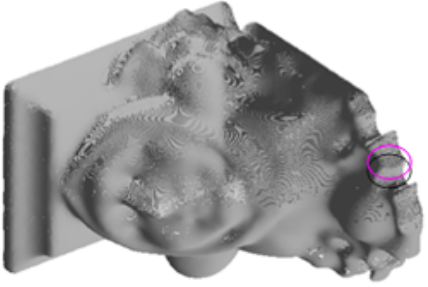



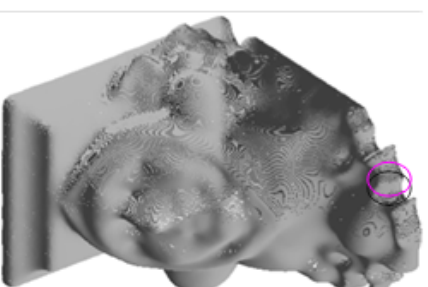





Point cloud

Sliced model

Fabricated model

Manufacturing compatibility with different layer thickness

	AM System Compatibility	Sliced model		Support structure	Manufactured model
		Global view	Local view 0.1mm		
Macro →	Option A <u>Platform size</u> 260 X 160 mm <u>XY resolution</u> 0.14 mm <u>Z layer</u> 0.15 mm				
	Option B <u>Platform size</u> 48 X 36 mm <u>XY resolution</u> 0.047 mm <u>Z layer</u> 0.05 mm				
	Option C <u>Platform size</u> 14 X 10.5 mm <u>XY resolution</u> 0.014 mm <u>Z layer</u> 0.01 mm				

- Tele-fabrication is critical for future product design and manufacturing
- Developed a tele-fabricating approach by integrating 3D scanning and printing
- Presented a direct geometry data flow method in such an integration system
- Performed physical experiments to verify the effectiveness of the direct geometry method.

- National Science Foundation CMMI-0927397 (USC).
- National Science Foundation CMMI-0900597 and CMMI-1030347 (IIT)

Questions?

